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A NORMAL COMPONENT OF THE GAS FLAME SPEED

We study the burning of an open flame of hydrocarbon fuel in the air atmosphere and introduce a method of the flame speed normal component determination for a selected local diametrical slice. A distribution of the obtained values along the flame axis reveals the inner flame structure and its variation depending on the fuel-oxidant ratio.

Keywords: burning; hydrocarbon flames; normal component of the flame speed; local slices; flame structure

A search of the conditions for the efficient combustion of the fuel is one of the most important energy problems. In order to find such combustion modes, it is necessary to understand the mechanism of the burning process depending on the oxidant-fuel ratio, which may be described by the excess of the oxidant (air) α in the combustible mixture.

A mechanism of burning is closely related to the flame structure. For example, a pulse burning occurs at certain values of oxidant-fuel ratio α, which leads to the burning front degeneration into burning zone. The electric breakdown voltage in this zone is lower than that in the nearby volumes of the flame [1], and the temperature is higher [2]. This may suggest a more complete combustion and thus a more efficient fuel utilization.

It should be noted that the mentioned methods (temperature measurement using a thermocouple and breakdown voltage measurement) assume the flame scanning, which makes it impossible to obtain a snapshot of the entire flame structure at once. Existing optical methods are good for this purpose, but they require a complex experimental equipment [3].

An intensification of burning may be confirmed by an increase of the flame speed (more precisely, its normal component). The authors of [4] suggest a method of digital processing of the flame photographic images and calculate the integral (over an entire surface of the burning front) values of the normal flame speed.

Our method allows to determine the normal component of the local flame speed in any chosen diametrical slice of a flame.

In the present paper we study the burning of an open laminar (Re = 805) torch of the prepared example gas mixture (fuel: 40% propane + 60% butane; oxidant: air) above the upright burner. The value of Re was calculated as $Re = v \cdot d/\nu$, where v is the linear flow speed in the burner (measured with rotameters), d is the inner diameter of the burner, ν is the kinematic viscosity (the reference data taken from [5]).

The burning takes place in the air atmosphere under normal conditions (temperature 20 °C; pressure 768 mm Hg). The experimental setup as well as the flame structure and its changes depending on α are described in [1,2]. The fuel (propane-butane) and the air were supplied to the mixer unit using two separate pipes. In order to prevent the spontaneous ignition, the temperature of the mixer unit was at 310 K level, which is much less than the ignition temperature of 700 K. The experimental setup was similar to the one described in [1, 2]. Let us focus on the normal component of the linear burning velocity.

Fig. 1 shows the photographic images of the torches above the burner with the nozzle diameter of 0.8 cm. The brightest inner cone is bounded by the narrow region – the reaction front. Inside of this front is the region of the pre-burning preparation of the combustible mixture (heating, decomposition etc.). Outside is the after-burning region.

The combustible mixture consumption varied within 1.2%, so the changes of the flame structure were obviously determined by the change in α. The digital image processing was as follows: the digital photographs of a flame were binarized with certain brightness threshold much like it had been done in [4]. The difference is that we used a sum of all three channels (RGB). Thus obtained silhouette of a flame was sliced into a number of layers (blocks) with a constant vertical step (fig. 2a). The lateral area of each block was calculated in the conic frustum approximation. From the calculated Re value a laminar flow of the combustible mixture may be assumed. Consequently, dividing a total mixture flow L (measured with rotameters) by the cross-section area of the flame base S_0^{cross} (fig. 2b), we obtain specific mixture flow. Next, we take the difference between the cross-sections of the two adjacent slices ($S_{i-1}^{cross} - S_i^{cross}$) and multiply it by the specific mixture flow to obtain the mixture discharge through the selected slice. Dividing this value by the lateral area of the same slice S_i^{block} directly yields the normal component of the burning speed in the i^{th} local slice of the flame – V_i^n. Applying the same procedure for all slices, we obtain a distribution of the normal component of the burning speed along the torch.

$$V_i^n = \frac{L}{S_0^{cross}} \cdot \frac{(S_{i-1}^{cross} - S_i^{cross})}{S_i^{block}} \quad (1)$$

The proposed approach allows us to determine the value of V_i^n for the i^{th} local slice of certain (predefined by the experimental conditions) size within a flame. It lets one solve the problem of both the geometrical localization of the reaction zone, and determination of its size. As a limiting case, to find the average value of the flame speed normal component $\langle V^n \rangle$ for the inner cone as a whole.

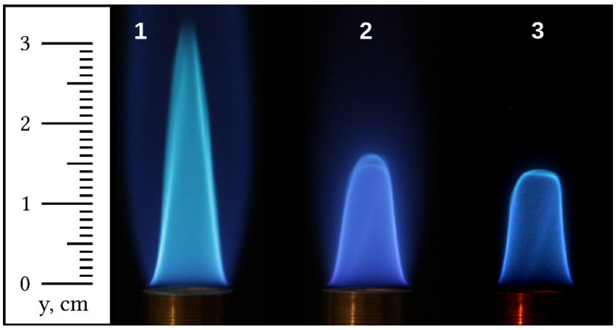

Fig. 1. Photographs of the inner cones of the propane-butane torch: 1) α=0.93; 2) α=1.3; 3) α=1.38.

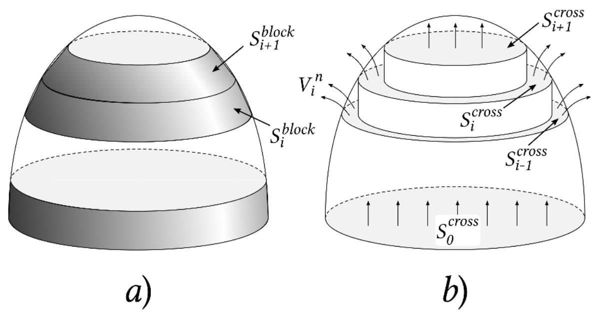

Fig. 2. An illustration of the slice parameters calculation.

The results are presented in fig. 3. The error of the V_i^n determination was estimated as follows:

$$\sigma_V \approx 2\pi RL \cdot (S_0^{cross})^{-2} \sigma_R, \quad (2)$$

where R is the flame cross-section radius, σ_R is the error of the radius measurement by the image ($\sigma_R \approx 0.02\ cm$).

An average normal component of the flame speed $\langle V^n \rangle$ was also estimated from the lowest cross-section area (S_0^{cross}) and the total lateral area (S_0^{cap}). By taking the $\langle V^n \rangle$ as a reference value for each studied flame, it is possible to single out two distinctive zones: a) near the base of the inner cone, where it first touches the ambient (secondary) air; b) at the top of the inner cone.

The zone a) is characterized by the influence of the ambient (secondary) air, which is reflected by the increased values of V_i^n relative to $\langle V^n \rangle$. This influence decreases as the α increases (transition from curve 1 to curve 3 in fig. 3.)

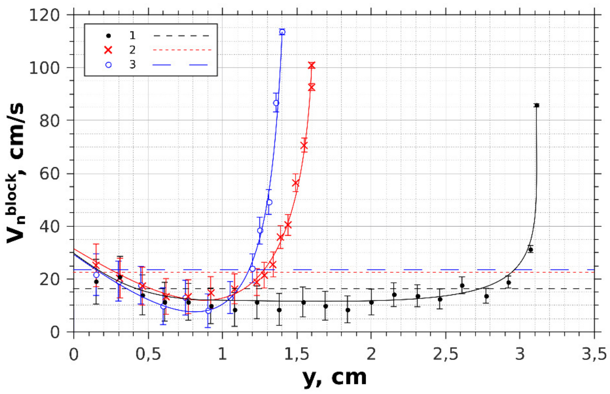

Fig. 3. Distribution of the normal component of the local flame speeds along the torch for: 1) α=0.93; 2) α=1.3; 3) α=1.38. The dashed lines mark the corresponding average values $\langle V^n \rangle$: 1 – 13.6 cm/s; 2 – 22.6 cm/s; 3 – 23.6 cm/s.

As of the zone b), the local flame speeds increase with α because of the growing role of the kinetic reactions – both due to the excess of oxidant and higher temperatures [2] (leading to a deeper decomposition of the initial propane and butane molecules). For the sake of comparison, a portion of the mixture which burns faster than $\langle V^n \rangle$ may be estimated. For α=0.93 this portion is 10%; for α=1.3 – 29%; for α=1.38 – 41%.

Thus, we suggest a method of determination of the local flame speed normal component V_i^n. Based on the obtained results, one may single out two zones within the inner cone of the flame where local flame speeds are higher than $\langle V^n \rangle$: near the base of the torch and at the top of the torch. The higher V_i^n at the base of the cone are probably related to the contact with the ambient air, with its influence decreasing as α increases. The higher values of V_i^n at the top of the cone may be caused by the kinetic reactions with their role increasing as α increases.

1. M.Yu. Trofimenko, S.K. Aslanov, V.P. Smolyar, Electrical structure of the jet of a gas mixture flame, Surface Engineering and Applied Electrochemistry, **50** (3),275-279 (2014).
2. M.Yu. Trofimenko, S.K. Aslanov, V.P. Smolyar, Structural changes in the gas flame upon the pulsating combustion mode onset, Ukrainian Journal of Physics, **59** (4), 359-364 (2014).
3. A. Popov, A. Tyurin, V. Tkachenko, A. Bekshaev, V. Kalinchak, M. Trofimenko, Speckle-Interferometric Approach to Flame Diagnostics, Imaging and Applied Optics 2015, OSA Technical Digest (online) (Optical Society of America, 2015), paper JT5A.43.
4. В.В. Калинчак, Ф.Ф. Каримова, С.Г. Орловская, М.С. Шкоропадо, Обработка изображений для определения скорости горения, 16-я Международная конференция «Цифровая обработка сигналов и её применение – DSPA-2014», Москва, Россия, доклады Том 2, стр. 449-452.
5. Н.В. Варгафтик. Справочник по теплофизическим свойствам газов и жидкостей. Москва. 1963г. С. 708.

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НОРМАЛЬНА СКЛАДОВА ШВИДКОСТІ ГОРІННЯ ГАЗОВОГО ФАКЕЛА

Досліджено горіння відкритого факела вуглеводневого палива у повітряній атмосфері. Запропоновано методику визначення нормальної складової швидкості горіння виділених локальних об'ємів факела. Показано, що розподіл швидкостей уздовж факела полум'я (внутрішнього конуса) виявляє структуру факела та її зміну в залежності від співвідношення окисник – паливо у початковій пальній суміші.

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НОРМАЛЬНАЯ СОСТАВЛЯЮЩАЯ СКОРОСТИ ГОРЕНИЯ ГАЗОВОГО ФАКЕЛА

Исследовано горение открытого факела углеводородного топлива в воздушной атмосфере. Предложена методика определения нормальной составляющей скорости горения выделенных локальных объёмов факела. Показано, что распределение скоростей вдоль факела пламени (внутреннего конуса) выявляет структуру факела и ее изменении в зависимости от соотношения окислитель – горючее в исходной горючей смеси.