

РОЗДІЛ 2

ЕНЕРГЕТИКА ТА ЕНЕРГОЗБЕРЕЖЕННЯ

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ENERGY EFFICIENT TRANSFORMERS WITH VARIOUS LOAD GRAPHICS FOR THE CONSUMERS OF ELECTRIC POWER

The development and implementation of a new economic electrical equipment, in particular, energy-efficient distribution transformers – is a very essential step to reduce electricity losses in 0,4-35kV distribution networks. In a market economy the funds invested into the sector of energetics provide maximum profit to the joint stock company only in the case of the production profitability. In such a situation it is possible to achieve optimal material and energy costs on the transformation of power only under the condition of taking into account such factors as load charts of electricity consumption, the cost of the electrical power losses and maintenance of transformers in the process of exploitation, etc. Existing until today practice of transformers design ignores the actual characteristics of individual customers load charts that results in inefficient use of power transformers capacities during their operation. Non-consideration of the electroconsumer actual operating mode (load curve) in the design period leads to inefficient use of transformer capacity. It is proposed for a tight load schedule to design the transformer for the nearest least normalized power compared to the actual load, providing the possibility of intensification of cooling in case of power consumption increasing.

Key words: Transformer; Power consumption; Load; Capacity; Distribution networks.

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ЕНЕРГОЕФЕКТИВНІ ТРАНСФОРМАТОРИ ДЛЯ ЕЛЕКТРОСПОЖИВАЧІВ З РІЗНИМИ ГРАФІКАМИ НАВАНТАЖЕННЯ

Неврахування при проектуванні дійсного режиму роботи (графіка навантаження) електроспоживачів призводить до неефективного використання трансформаторної потужності. Пропонується при поганому графіку навантаження спроектувати трансформатор на найближчу меншу нормалізовану потужність у порівнянні з реальним навантаженням, при цьому передбачити можливість інтенсифікації охолодження при збільшенні споживаної потужності.

Ключові слова: Трансформатор; Споживання енергії; Навантаження; Місткість; Розподільні мережі.



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INTRODUCTION

The development and implementation of a new economic electrical equipment, in particular, energy-efficient distribution transformers – is a very essential step to reduce electricity losses in 0,4-35 kV distribution networks.

In a market economy the funds invested into the sector of energetics provide maximum profit to the joint stock company only in the case of the production profitability. In such a situation it is possible to achieve optimal material and energy costs on the transformation of power only under the condition of taking into account such factors as load charts of electricity consumption, the cost of the electrical power losses and maintenance of transformers in the process of exploitation, etc.

Existing until today practice of transformers design ignores the actual characteristics of individual customers load charts that results in inefficient use of power transformers capacities during their operation.

Only recently some companies which manufacture transformers have begun to adhere to the principle of customization, which takes into account the requirements of a particular user (Kravchenko, 2013) [5].

Today's situation with the irrational utilization (mostly under-utilization) of transformer capacity can be explained by "operational" (e.g, industrial facilities like power consumers are in a stage of stagnation, etc.) and "design" (the wrong accounting of nominal load losses time of the transformer that was laid down in the design process) reasons.

For the rational utilization of transformers which are already in operation, if the actual loads do not match with the project ones (real load is generally less) it is necessary to replace the operating transformer on the lower power transformer without changing the cooling system.

Proper tracking of nominal load losses time at the transformer design stage will allow to increase the efficiency of its operation. Neglect of real operating conditions of customers at the design stage leads to damage associated either with overspending of investment (if the load is lesser than project one), or to the additional costs of electricity losses (if the load is more than the project one).

According to [1, 7, 11], it is possible to determine the number of shifts on the enterprise using the annual consumers operation number of hours with maximum load and annual energy consumption. The exploitation time interval of the transformer with a rated capacity is equal to 1800 ... 2500 (load factor $F_l = (0.2 \dots 0.3)$) for one-shift work, for two-shift work – 3500 ... 4500 ($F_l = 0.4 \dots 0.5$), for three-shift work – 5000 ... 7000 ($F_l = 0.55 \dots 0.8$). The modern series of distribution transformers of 1 and 2 dimensions is designed for average operational loads, typical for two-shift production schedule [10].

The main characteristics that define the technical and economic level of power transformers are power losses (of no-load operation and short-circuit). Levels of these losses, their relationship, characterize the operation mode of electric consumers.

One possible way of rational utilization of distribution transformers [7, 12] is the development of a series of transformers with different ratios of the no-load operation and short-circuits losses values. However, this path leads to the creation of an excessively large number of distribution transformers modifications.

In [6, 8] it was noted that for a small-time operation of a distribution transformer with a rated load it is necessary to use the transformer with a lesser capacity in order to save material and energy resources, providing for intensification of cooling in case of the transformer operation on a heavier load.

Computational studies has shown that for increasing the effect of the implementation in practice this type of distribution transformers it would be useful to introduce the intermediate sizes (power) transformers in modern domestic standard power ratings. This will create a series of distribution transformers with a scale pitch equal to 1.25 of the scale capacity used in the standard international practice [12]. Aligning national standards in line with the Harmonization Documents – HD which are the basis for the EN – European standard, which is required for a single European settlement of the issues of transformer is the actual task [13].

MATERIALS AND METHODS

In the framework of this article computational studies to determine the effectiveness of the use of the transformer, depending on the characteristics of the technological mode (shift) of the electroconsumer work were con-

ducted, necessary measures were determined for the rehabilitation of existing cooling systems through the use of additional oil coolers.

The criterion of discounted expenses was adopted at the design studies to assess the effectiveness of the technical solutions. These are the expenses on construction and exploitation of the transformer, considering the inflation processes in the economy, from the moment of determining the expenses for the whole period of operation [4, 9].

$$3_{\partial} = D_{\text{ЭКВ.Т}} \cdot K_{TP} + C_{xx} \cdot P_{xx} + \left(\frac{P_{\text{кз}}}{U_{\text{H}}^2} \right) \cdot S^2, \text{UAH}, \quad (1)$$

where

$D_{\text{ЭКВ.Т}} = (1+E)^{-1} + a_{\text{обсл}} \cdot D_{P\partial} - (1-a_{\text{пен}} \cdot T_{\partial}) \cdot (1+E)^{-T_p}$ – equivalent discount factor;

$D_{P\partial} = \sum_{t=1}^{T_p} (1+E)^{-t}$ – estimated discount factor for the

period of operation until the end of the estimated period;

$K_{TP} = K_{TP,\text{баз}} \cdot K_{\text{деф}}$ – the estimated cost of the transformer considering the inflation factor at the time of determination of expenses.

$a_{\text{обсл}}$ – coefficient of royalties for service and repair;

$a_{\text{пен}}$ – coefficient of royalties for renovation;

T_{∂} – operation period of the transformer;

E – standard of discounting;

T_p – duration of the calculation period;

$C_{xx} = C_e \cdot T_{\partial} \cdot D_{\text{п.э.}}$ – expenses on compensation for loss in the mode of idling;

C_e – electricity price;

T_{∂} – transformer activation time.

In carrying out these studies economic such economic parameters were adopted: standard of discounting = 0,1; calculation duration period = 10 years; deflation rate at the 2014 year level = 30; the price of electricity = 1,80 UAH/(kW·year).

As an example, two distribution transformers with adjacent capacity (increments of the scale were equal to 1,25) which are used today in generally accepted international practice were considered. Transformer operation at the less power in the modes in which the currents flowing in the windings of the transformer are commensurate with transformer currents of greater power, is accompanied by a significant increase in current density in the windings and thus increasing the level of losses in the transformer approximately on 25-35% [8].

Increase in the level of total losses for the transformer of less capacity running with a load close to the nominal of the higher power transformer (adjacent on power scale) in turn leads to higher winding temperatures and consequently to the need in performing technical measures aimed at maintaining the thermal state of the transformer within rules laid down in [2, 3].

The most appropriate way to intensify the cooling (forcing) is the connection of additional cooling devices to an existing cooling system. This is explained by the

fact that the industry has mastered the production of radiators with any number of cooling tubes. With proper selection of the number of cooling pipes in the radiators it is always possible to achieve the required degree of cooling boost.

The cost of the transformer is the sum of the values of the active part and the cost of the cooling system:

$$U_{TP} = U_{a.c.} + U_{oxl} \quad (2)$$

Additional financial expenses for intensification of cooling are determined according to the expression:

$$\Delta U_{\phi} = (P_{XX2} - P_{XX1}) \cdot T_B \cdot C_3 + (P_{K32} \cdot \tau_2 \cdot C_3 - P_{K31} \cdot \tau_1 \cdot C_3)$$

where P_{XX2}, P_{K32} – losses levels (respectively idling and short circuit) of the transformer with a less magnitude capacity than the actual operating load, kW;

P_{XX1}, P_{K31} – losses levels (respectively idling and short circuit) of the transformer with equal to or greater magnitude capacity than the actual operational load, kW;

T_B – transformer activation time, hours;

τ_1, τ_2 – transformer operation time at the nominal load, respectively of higher and lower capacity;

C_3 – the price of electrical power, UAH/kw-hour.

In turn the cost of the cooling system

$$U_{oxl} = C_{oxl} \cdot (P_{K3} + P_{XX})$$

where C_{oxl} – specific cost of losses compensation.

In the market conditions the transformer cooling devices production cost from different manufacturers of transformer equipment may vary by 20-30%. In order not to become attached to the cost indexes of a specific producer maximum values of $C_{oxl,max}$ cooling devices specific cost were determined, to compensate the increase in the transformer total losses (at the loads in magnitude of transformer higher nominal power).

The maximum values of additional cooling devices specific cost – i.e. the limit values at which the production and operation expenses of the less power transformers are the same with high power transformer without additional cooling devices. In high load conditions due to the use of additional cooling devices the lifetime of insulating materials remains unchanged.

The results of computational experiment for one pair of adjacent power transformers are given in Table 1.

Table 1 – Technical and economic parameters of the less power transformer when it is operating with the relevant higher power transformer loads

Technical and economic parameters	$S_H = 320$ kV·A	Geometry $S_H = 320$ kV·A. Load (currents) $S_H = 400$ kV·A; Steel (3406) = 15 UAH/kg; Copper = 60 UAH/kg						$S_H = 400$ kV·A
		The load of higher power transformer (operation mode)						
		one-shift		two-shift		three-shift		
		0,2	0,3	0,4	0,5	0,6	0,65	
MO, mm	323	323	323	323	323	323	323	333
D, mm	165	165	165	165	165	165	165	175
H, mm	520	520	520	520	520	520	520	552
U_k , %	4,5	5,78	5,78	5,78	5,78	5,78	5,78	4,5
G_{CU} , kg	278	278	278	278	278	278	278	310
G_{MAG} , kg	450	450	450	450	450	450	450	523
Z_d , UAH/year	7440	6585	7042	7499	7955	8440	8615	8618
$C_{a.c.}$, UAH	24244	24244	24244	24244	24244	24244	24244	27333
P_{K3} , W	4458	6925	6925	6925	6925	6925	6925	5557
P_{XX} , W	709	709	709	709	709	709	709	826
P_{K3}/P_{XX} , W	6,29	9,77	9,77	9,77	9,77	9,77	9,77	6,72
J_{HH}/J_{BH} , A/mm ²	<u>2,75</u> 2,25	<u>3,35</u> 2,85	<u>3,35</u> 2,85	<u>3,35</u> 2,85	<u>3,35</u> 2,85	<u>3,35</u> 2,85	<u>3,35</u> 2,85	<u>2,8</u> 2,45
t_{HH}/t_{BH} , °C	<u>16,7</u> 16,1	<u>22,4</u> 22,5	<u>22,4</u> 22,5	<u>22,4</u> 22,5	<u>22,4</u> 22,5	<u>22,4</u> 22,5	<u>22,4</u> 22,5	<u>17,6</u> 17,7
$P_{cym} = P_{XX} + P_{K3}$, W	5167	7634	7634	7634	7634	7634	7634	6383
$\Delta P_{cym} = P_{cym 320} - P_{cym 400}$, W		1251	1251	1251	1251	1251	1251	0
$\Delta Z_d = Z_{d320} - Z_{d400}$, UAH/year		-2033	-1576	-1119	-663	-178	-3	0
$C_{oxl}(Z_d)_{max}$, UAH/kW		1625	1260	895	530	143	2	
n_{oxl}	2				3			3
t_{mac} , °C	38,4				41,7			35,8
ΔK , UAH					896			
C_{oxl} действ., UAH/kW					716			

Graphic interpretation of computational research is shown in Figure 1 as a function $C_{\text{охл,макс}} = f(S_H, K_3)$. According to this relationship we can determine the maximum value of the specific value (UAH/kW) of additional cooling devices for a given power transformer and its operation mode (shift), in which the manufacture and operation of power transformers related costs will be the same.

In view of the prices [14, 15] of structural steel (8 UAH/kg) and transformer oil (15 UAH/kg) of addi-

tional capital investments for the cooling intensification are $\Delta K = U_{\text{стохл}} \cdot G_{\text{стохл}} + U_{\text{мохл}} \cdot G_{\text{мохл}}$ for radiators with the following distance between flanges:

- 710 mm: $\Delta K_{710} = 8 \cdot 34,14 + 15 \cdot 24 = 585,12 \approx 586$ UAH;
- 900 mm: $\Delta K_{900} = 8 \cdot 41,14 + 15 \cdot 30 = 719,12 \approx 720$ UAH;
- 1150 mm: $\Delta K_{1150} = 8 \cdot 50,14 + 15 \cdot 38 = 895,12 \approx 896$ UAH;
- 1400 mm: $\Delta K_{1400} = 8 \cdot 53,94 + 15 \cdot 46 = 1029,52 \approx 1030$ UAH.

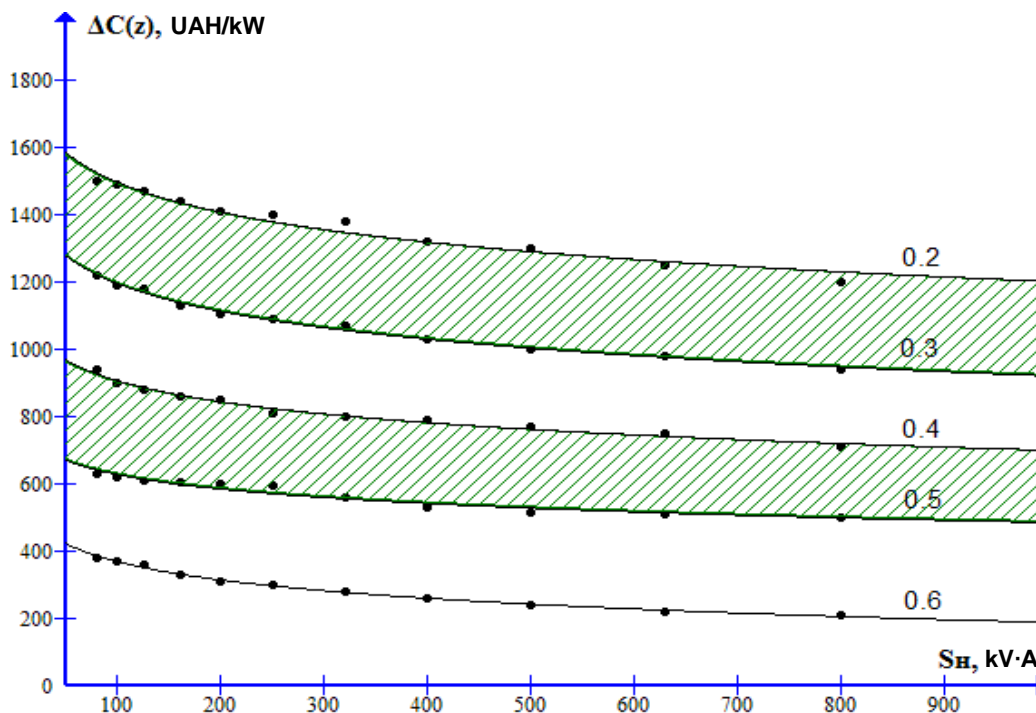


Figure 1 – Values ranges of the specific cost of additional cooling devices, which provide economic benefit from the use of transformers.

The analysis the catalog data of different manufacturers of transformer equipment shows that the weight of the transformer oil in tanks of adjacent power transformers differs by about 20-30 kilograms (with a power range $S_H = 100-500$ kVA) and 30-80 kilograms (with a power range $S_H = 500-1000$ kVA). This allows you to obtain additional economic benefit of $E_{\text{д}} = (20..30) \cdot 15 = (300..450)$ UAH, at a power transformer $S_H = 100-500$ kVA и $E_{\text{д}} = (30..80) \cdot 15 = (400..900)$ UAH, at a transformer power $S_H = 500-1000$ kVA.

RESULTS AND DISCUSSION

1. To create energy-efficient transformers with optimum technical and economic parameters it is necessary at the design stage follow the principle of customization, which takes into account features of the schedule loads and requirements of specific electroconsumer for which they are being developed.

2. Standard or specific graphs of loads should be the basis for determining the optimal technical and economic parameters of transformers. Neglect in the design of the actual operating mode (load curve) of electroconsumer leads to inefficient use of transformer capacity.

3. The underutilization of transformer capacity by load loss requires the use of lower power transformers in comparison with the actual load and the use of intensification (boost) when the transformer cooling modes with power consumption higher than the nominal value.

4. The series of transformers produced today with a sufficiently large pitch (about 1.6) on a scale rated power does not allow the use of a transformer at rated power (of the two adjacent row on the normalized power) at the actual load of power consumer for (25-30)% less than the nominal capacity of the higher power transformer.

5. It is proposed the approach to the original design and the use of transformers with reduced power (on the normalized row) compared with the actual load and the more intensive use of the cooling system during operation of the transformer in nominal mode corresponding to the

nearest greater capacity on the normalized row, and in an overload mode .

6. To increase the effect of the introduction into practice this activity it is expedient to introduce the intermediate sizes of (power) transformers into the modern national standard of power ratings with 1.25 increment. This will allow to introduce the power scale, applied currently abroad.

REFERENCES

1. **Bystritskiy, G.F.** (2003). *Vybor i ekspluatatsiia silovykh transformatorov*. Moscow, Izdatelskiy tsentr «Akademiya», 176 p.
2. GOST 14209-97(MEK 354-91). *Mezhhgosudarstvennyy standart. Rukovodstvo po nagruzke silovykh maslianykh transformatorov*. (Data vvedeniia 2002.01.01).
3. DSTU 3645-97 (GOST 3484.2-88) (IEC 60076-2:1993) *Transformatori silovi. Dopustymi perevyschennia temperatury ta metody vyprovuvannia na nagrivaniiia-Chinniy vId 2000-07-01*, 35 p.
4. **Zuev, E.N.** (2002). K voprosu ob aktualizatsii normativov na ekonomicheskuiu plotnost toka. *Elektro*, No. 6.
5. **Kravchenko, A.N., Metelskiy, V.P.** (2013). *Maslianye energoefektivnyye transformatory*. *Elektrik*, No. 5.
6. **Matuhno, V.A.** (2009). Designing transformers according to their exploitation load. *Electrical machine-building and electrical equipment*, iss. 73, 97-101.
7. **Pekelis, V.G. Myshkovets, E.V., Leus, Yu.V.** (2003). *Opreделение optimalnykh urovnei poter kholostogo khoda i korotkogo zamykaniia dlia razlichnykh rezhimnykh usloviy raboty transformatorov moschnosti do 1600 kVA*. *Elektro*, No. 1, 42-46.
8. **Puylo, G.V., Chaykovskiy, V.P., Matuhno, V.A.** (2013). *Seriia optimalnykh transformatorov dlia elektropotrebitel'ei s razlichnymi grafikami nagruzki*. *Nauka v Informatsionnomu prostori: IX int. scien. conf.* (10–11 October 2013), URL: http://www.confcontact.com/2013-nauka-v-informatsionnom-prostranstve/tn6_pujlo.htm. Date of access: 02.02.2016.
9. **Savintsev, Yu.M., Karamutdinov, R.N.** (2010). *Vybor silovogo transformatora – delo serioznoie* [Electronic source]. Available at: <http://www.energyland.info/analytic-show-56794>. Date of access: 02.02.2016.
10. **Tihomirov, P.M.** (1986). *Raschet transformatorov*. Moscow, Energoatomizdat, 528 p.
11. **Shidlovskiy, A.K., Vagin, G.Ya., Kurennyiy, E.G.** (1992). *Raschety elektricheskikh nagruzok sistem elektro-snabzheniia promyshlennykh predpriiaty*. Moscow, Energoatomizdat, 224 p.
12. *Energosberezhenie v Evrope: primenenie energoefektivnykh raspredelitelnykh transformatorov [izdanie Evropeyskogo instituta medi (Tema «B» sovmestno s Evropeyskoy Komissiey proekta No. STR-1678-98-BE), per. s angl. E. V. Melnikova]. Energosberezhenie, 1'2004*. Available at: http://www.abok.ru/for_spec/articles.php?nid=2384. Date of access: 02.02.2016.
13. HD 428 (Harmonization Documents): *Trekhfaznyye raspredelitelnyye transformatory s rabochey chastotoi 50 Hz ot 50 do 2 500 kV·A s maslianykh okhlazhdeniem i maksimalnym napriazheniem ne vyshe 36 kV*. [Electronic source]. Available at: http://www.abok.ru/for_spec/articles.php?nid=2384. Date of access: 02.02.2016.
14. *Stali i splavy korrozionno-stoykie i spetsialnyye v Ukraine* [Electronic source]. Available at: <http://www.ua.all.biz/stali-i-splavy-korrozionno-stojkie-i-specialnye-bgr1553>. Date of access: 02.02.2016.
15. *Transformatornyye masla* [Electronic source]. Available at: <http://odessa.pulsen.com.ua/price/040119-transformatornye-masla>. Date of access: 02.02.2016.

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ЭНЕРГОЭФФЕКТИВНЫЕ ТРАНСФОРМАТОРЫ ДЛЯ ЭЛЕКТРОПОТРЕБИТЕЛЕЙ С РАЗЛИЧНЫМИ ГРАФИКАМИ НАГРУЗКИ

Неучет при проектировании действительного режима работы (графика нагрузки) электропотребителя приводит к неэффективному использованию трансформаторной мощности. Предлагается при неплотном графике нагрузки спроектировать трансформатор на ближайшую меньшую нормализованную мощность по сравнению с реальной загрузкой, при этом предусмотреть возможность интенсификации охлаждения при увеличении потребляемой мощности.

Ключевые слова: Трансформатор; Потребляемая мощность; Нагрузка; Вместимость; Распределительные сети.

ЛИТЕРАТУРА

1. **Быстрицкий Г.Ф.** Выбор и эксплуатация силовых трансформаторов [Текст] / Г.Ф. Быстрицкий. – М.: Издательский центр «Академия». – 2003. – 176 с.

2. GOST 14209-97(MЭК 354-91). *Межгосударственный стандарт. Руководство по нагрузке силовых масляных трансформаторов* [Текст]. (Дата введения 2002.01.01).

3. ДСТУ 3645-97 (ГОСТ 3484.2-88) (IEC 60076-2:1993) Трансформатори силові. Допустимі перевищення температури та методи випробування на нагрівання. – Чинний від 2000-07-01. – 35 с.
4. **Зуев Э.Н.** К вопросу об актуализации нормативов на экономическую плотность тока [Текст] / Э.Н. Зуев. – Электро. – 2002. – № 6.
5. **Кравченко А.Н.** Масляные энергоэффективные трансформаторы [Текст] / А. Н. Кравченко, В.П Метельский – Электрик. – 2013. – № 5.
6. **Матухно В.А.** Проектирование оптимальных трансформаторов для различных эксплуатационных нагрузок [Текст] / В.А. Матухно // – Электромашиностроения та електрообладнання. – 2009. – Вип. 73. – С. 97-101.
7. **Пекелис В.Г.** Определение оптимальных уровней потерь холостого хода и короткого замыкания для различных режимных условий работы трансформаторов мощностью до 1600 кВА [Текст] / В.Г. Пекелис, Е.В. Мышковец, Ю.В. Леус // – Электро. – 2003. – № 1. – С. 42-46.
8. **Пуйло Г.В., Чайковский В.П., Матухно В.А.** Серия оптимальных трансформаторов для электропотребителей с различными графиками нагрузки. Наука в інформаційному просторі : матеріали ІХ Міжнар. наук.-практ. конф., 10–11 жовт. 2013 р. : у 8 т. – Т. 3 : Технічні науки. – Дніпропетровськ, 2013. – 119 с. URL: http://www.confcontact.com/2013-nauka-v-informatsionnom-prostranstve/tn6_pujlo.htm
9. **Савинцев Ю.М., Карамутдинов Р.Н.** Выбор силового трансформатора – дело серьезное [Электронный ресурс]. Режим доступа: <http://www.energyland.info/analytic-show-56794>.
10. **Тихомиров П.М.** Расчет трансформаторов. Учебное пособие для вузов: издание пятое, переработанное и дополненное [Текст] / П.М. Тихомиров. – М.: Энергоатомиздат. – 1986. – 528 с.
11. **Шидловский А.К.** Расчеты электрических нагрузок систем электроснабжения промышленных предприятий [Текст] / А.К. Шидловский, Г.Я. Вагин, Э.Г. Куренный. – М.: Энергоатомиздат. – 1992. – 224 с.
12. Энергосбережение в Европе: применение энергоэффективных распределительных трансформаторов [Электронный ресурс] /Издание Европейского института меди (Тема «В» совместно с Европейской Комиссией проекта № STR-1678-98-BE), пер. с англ. Е. В. Мельникова // – Энергосбережение. – 2004. – № 1. Режим доступа: http://www.abok.ru/for_spec/articles.php?nid=2384.
13. HD 428 (Harmonization Documents): Трехфазные распределительные трансформаторы с рабочей частотой 50 Гц от 50 до 2 500 кВ·А с масляным охлаждением и максимальным напряжением не выше 36 кВ. [Электронный ресурс]. Режим доступа: http://www.abok.ru/for_spec/articles.php?nid=2384.
14. Стали и сплавы коррозионно-стойкие и специальные в Украине [Электронный ресурс. Режим доступа: <http://www.ua.all.biz/stali-i-splavy-korrozionno-stojkie-i-specialnye-bgr1553>].
15. Трансформаторные масла [Электронный ресурс]. Режим доступа: <http://odessa.pulsen.com.ua/price/040119-transformatornye-masla>].

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